

## Thermal fatigue degradation effects occurred at austenitic T connections:

- cyclic feeding (Civaux, FR)
- valve leakage (GKN, DE)

## Potential consequences?

- surface stresses
- crack initiation
- stresses in wall
- crack propagation

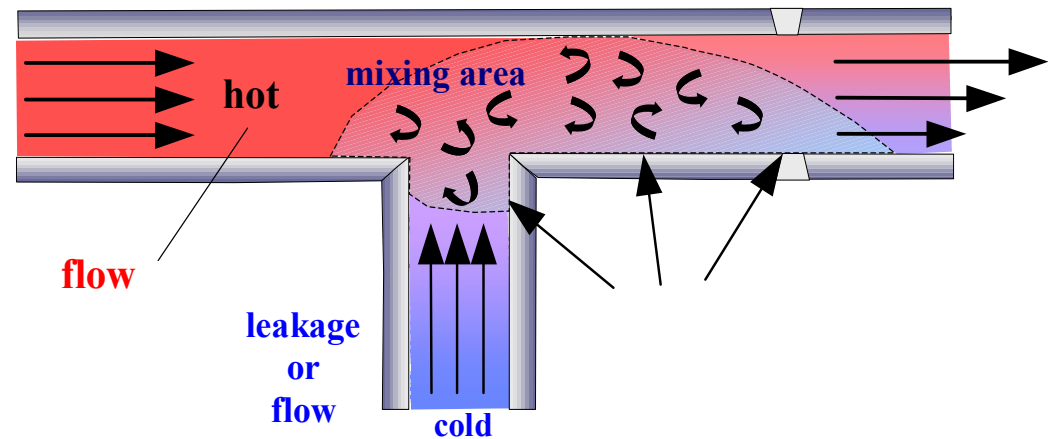
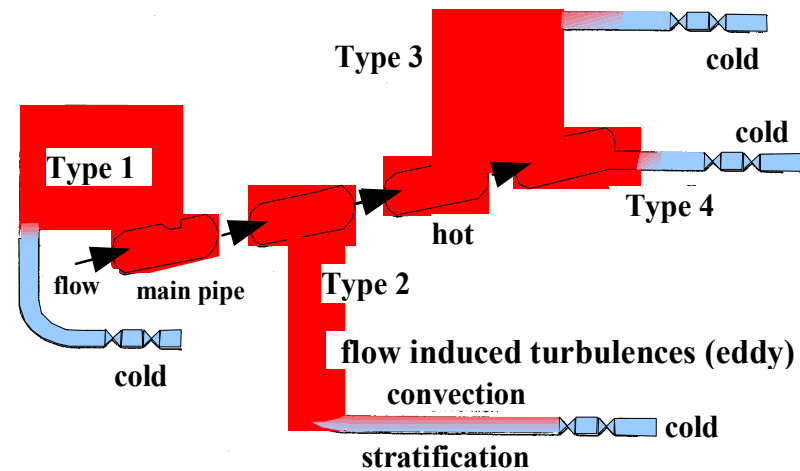


Figure 1: Turbulent mixing effects in piping system T connections

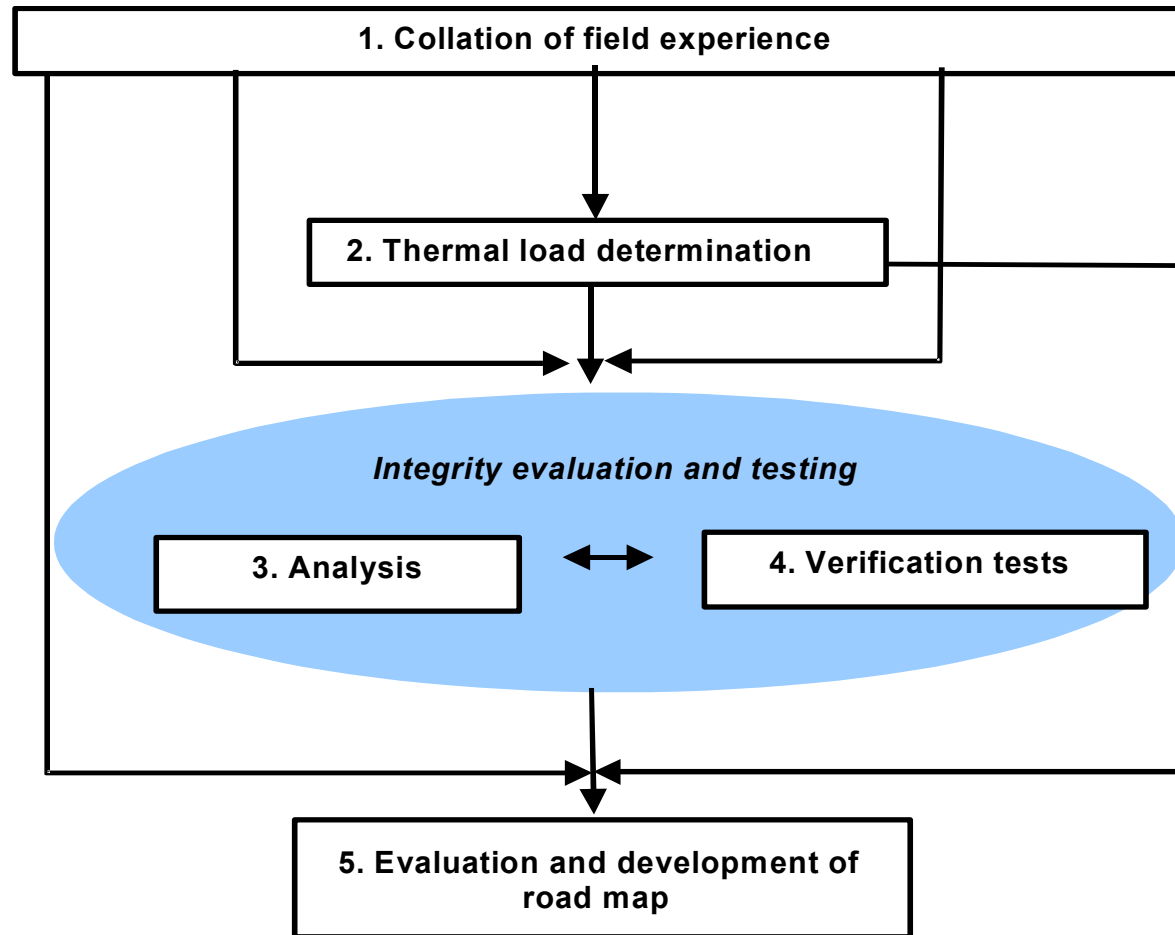


Figure 2: Work packages flow chart

<b>Name</b>	<b>Country</b>	<b>Organisation</b>
Wilke, U.	Germany	E.ON
Faidy, C.	France	EDF
Le Duff, J. A.	France	FANP-F
Braillard, O.	France	CEA
Cueto-Felgueroso, C.	Spain	Tecnatom
Varfolomeyev, I.	Germany	FHG
Solin, J.	Finland	VTT
Schippers, M.	Germany	FANP-D
Stumpfrock, L.	Germany	MPA
Nilsson, K.-F.	Netherlands	JRC
Vehkanen, S.	Finland	FNS
Seichter, J.	Germany	SPG
Abbas, T.	United Kingdom	CINAR
Figedy, S.	Slovakia	VUJE
Carmena, P.	Spain	ENDESA
Cizelj, L.	Slovenia	JSI

**Figure 3: THERFAT consortium**

## Temperature loads

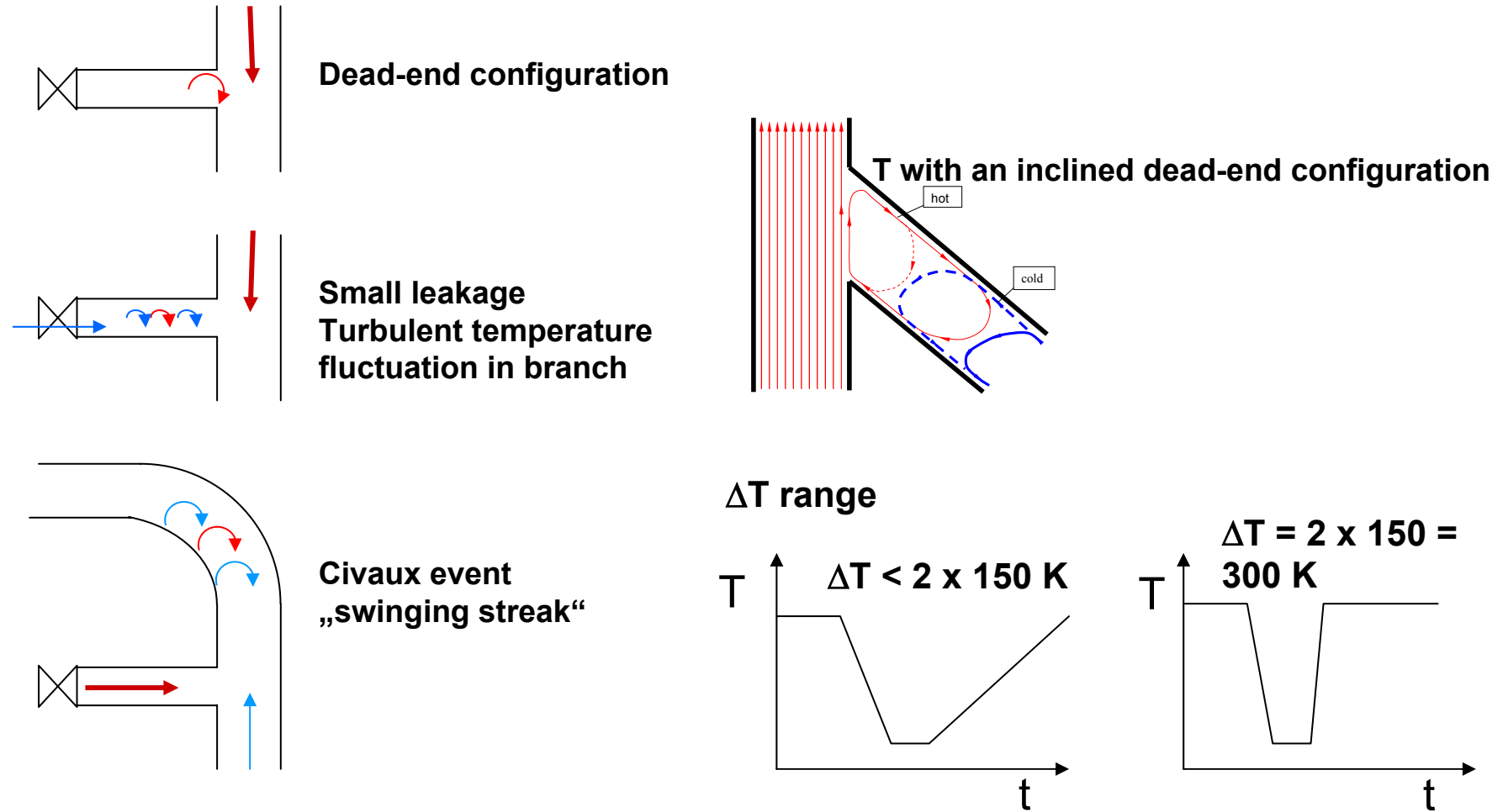
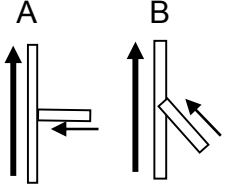
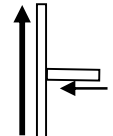


Figure 4: Field experience on high cyclic turbulent temperature mixing

Dimensions of T	Objective	Parameters	Remarks	Status
50 x 50 (90°-T)	Flow Visualisation	Various Flow Directions and Mass Flows	Tests at Room Temperature → Variation of Fluid Density 	Tests finished
50 x 50 (45°-T)	Flow Visualisation	Various Flow Directions and Mass Flows		
70 x 24 (90°-T)	Flow Visualisation	Various Flow Directions and Mass Flows		
100 x 100 (90°-T)	Flow Visualisation	Flow Direction A Mass Flows see table below		Tests finished
50 x 50 (90°-T)	Electric Conductivity Measurement	Main Flow in kg/s: 2 and 4  Leak Flow in kg/s: 0.03, 0.06 and 0.12	Tests at Room Temperature → Variation of Fluid Density 	Tests finished
		Main Mass Flow in kg/s	Leak Mass Flow in kg/s	
DN 100 x 100 (d <sub>i</sub> = 100)		20 10	0.015 0.03	

**Figure 5: SPG, glass models test matrix**

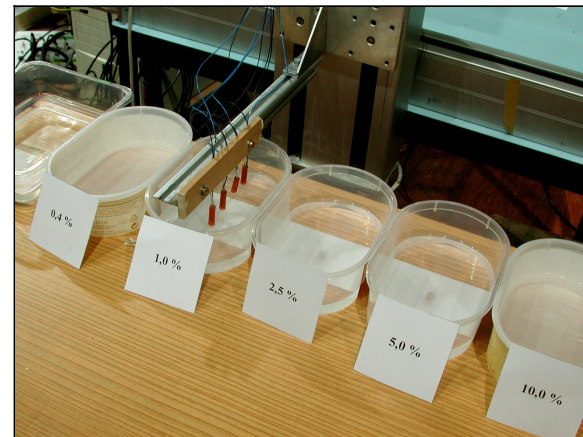
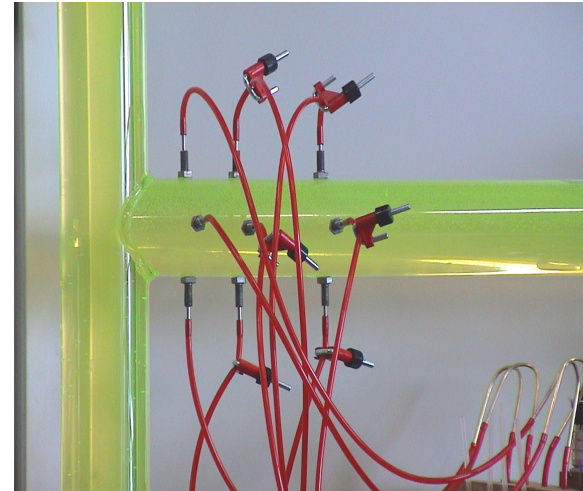
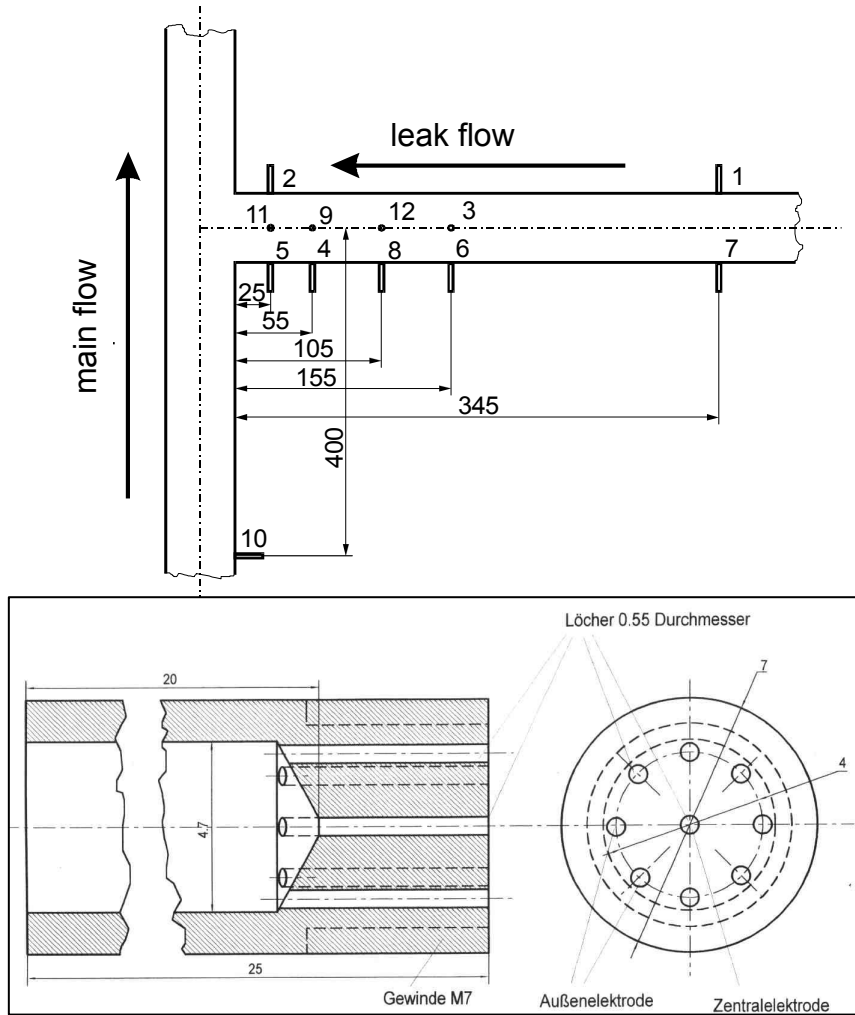
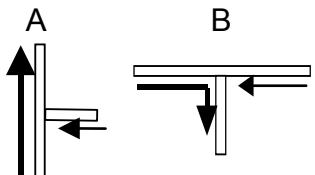
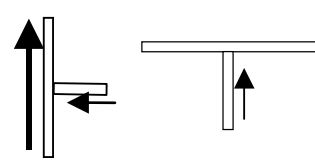


Figure 6: SPG, glass model, electrical conductivity measurement

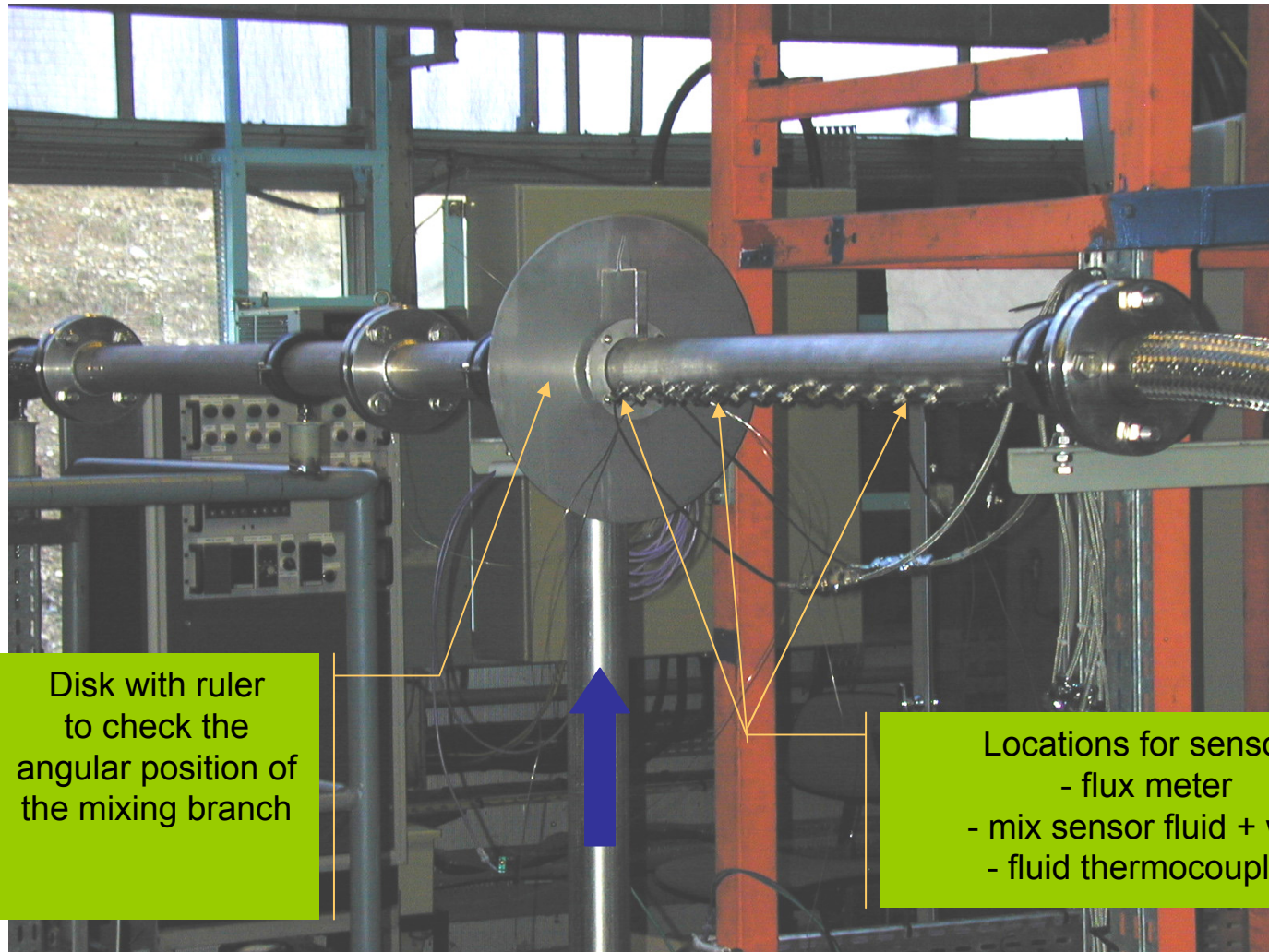
## Steel models (pipe wall thickness 1 mm)

### Test matrix

	T and flow orientation	Main mass flow $\dot{m}$ in kg/s	Leak mass flow $\dot{m}_l$ in kg/s	Temperature difference (hot – cold water) $\Delta T$ in K	Circumferential measurement position	Status
DN 50 x 50 ( $d_i = 48$ )		3,9 1,95	0.015 0.03 0.06 0.12 0.23	90 45	6 ... 12 o'clock	Tests finished
DN 80 x 20 ( $d_i = 78 \times 20$ )		5,5 2,75	0.015 0.03 0.06 0.12	90 45	6 ... 12 o'clock	Tests finished

**Figure 7: SPG, steel models, test matrix**

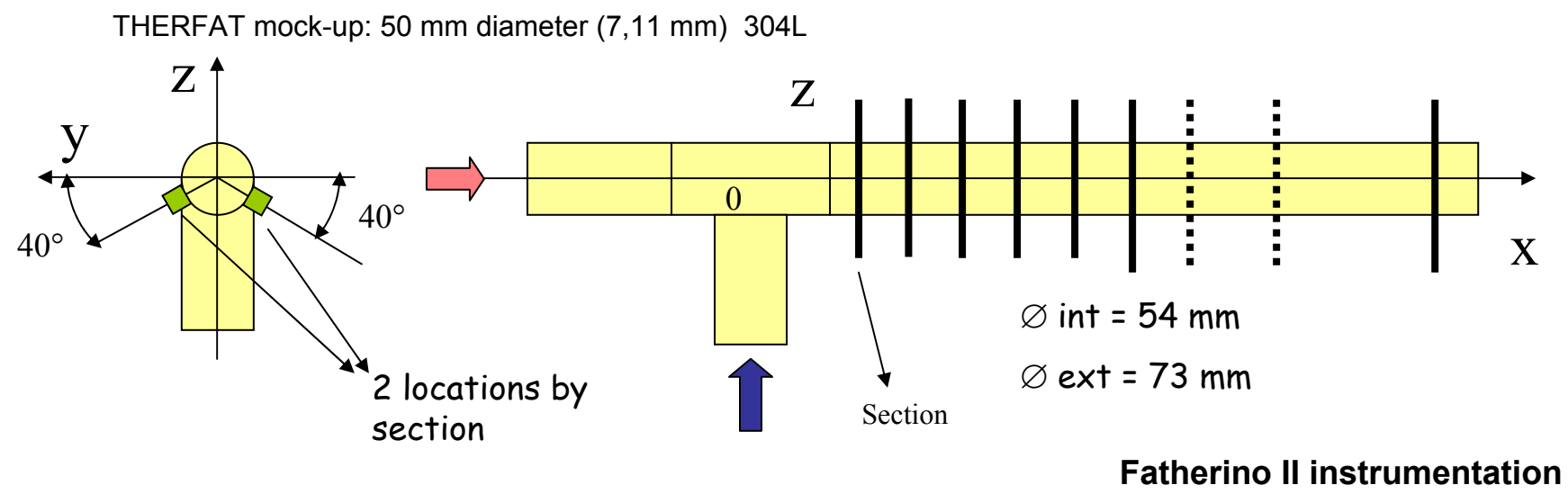
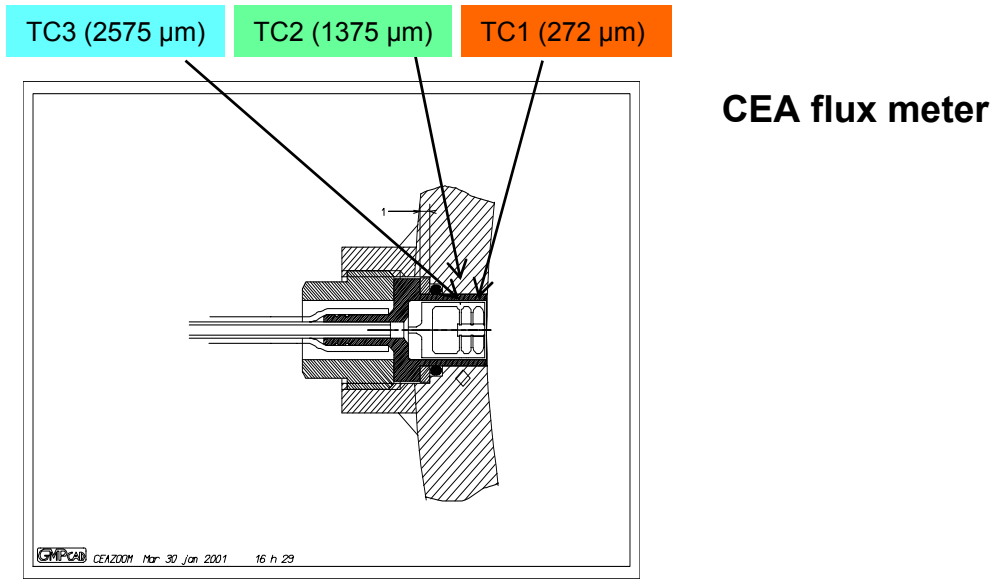
# The THERFAT mock-up



## Fatherino facility overview

Figure 8: CEA, Fatherino II experiment, test rig





**Figure 9: CEA, Fatherino II, test configuration**

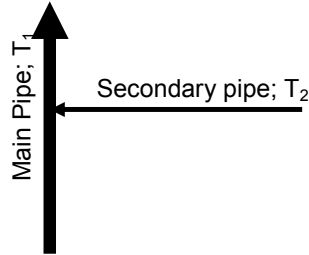
# THERFAT

## Example: turbulent-temperature load spectrum in branch

Measured temperature ranges – rain-flow evaluation

Vertical T 50 x 50 (wall thickness = 1 mm)

Measuring position 6 o'clock



Measured temperature ranges – rain-flow evaluation

Vertical T 50 x 50 (wall thickness = 1 mm)

Measuring position 6 o'clock

Secondary pipe, fluid temperature

Secondary pipe, outside wall temperature

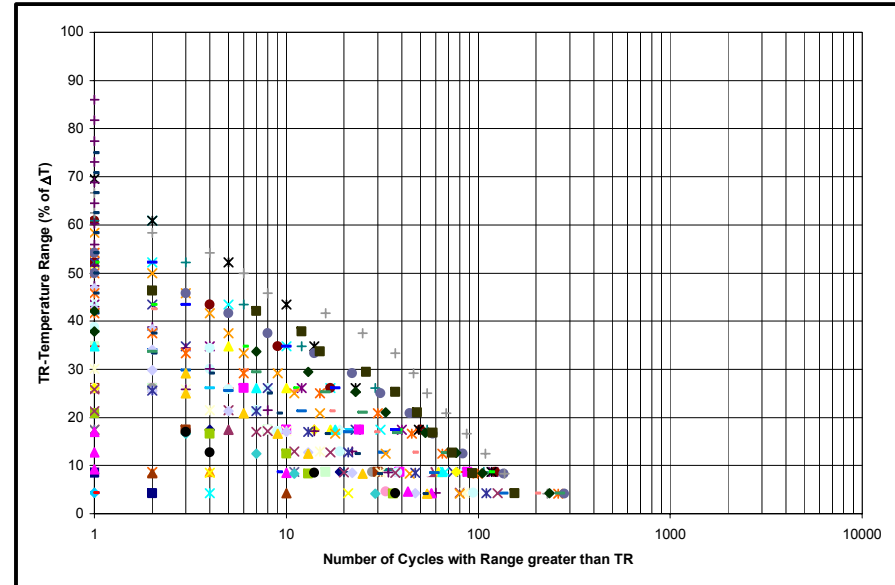
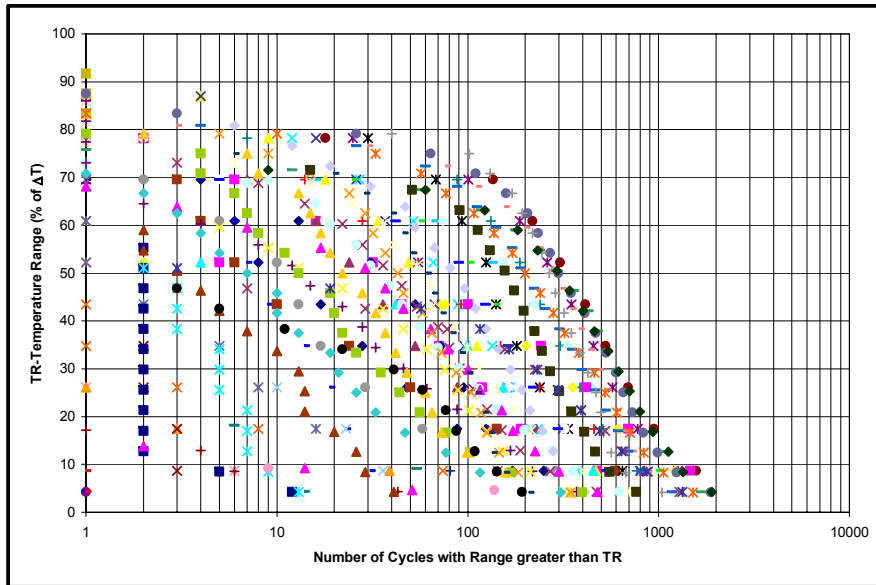


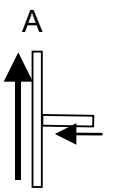
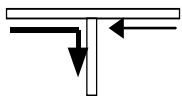
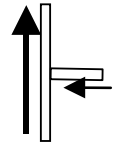
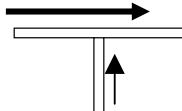
Figure 10: SPG, steel model, turbulent-temperature load spectrum

## Thermo-hydraulic tests on steel models (50 x 50 and 80 x 20)

- Steady flow in main pipe - one leg locked (closed valve) but leakage
- Temperature difference  $\Delta T$  (main flow – leakage) up to 90 K
- Temperature measurement outside and inside the wall (thickness 1 mm)

### Results

- Temperature alterations, load spectra (percentage of  $\Delta T$ )
- Mean heat-transfer coefficients found by inverse temperature calculation
- Report BLP-SB/27-04

T and flow orientation	Temp. alterations	Heat-transfer coefficient
DN 50 x 50 ( $d_i = 48$ ) <div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;"> <b>A</b>   </div> <div style="text-align: center;"> <b>B</b>   </div> </div>	Dead leg: > 90 % Main flow: $\leq 70$ %	Dead leg: $\leq 4000$ W/m <sup>2</sup> K (A) $\leq 7000$ W/m <sup>2</sup> K (B) Main flow: $\leq 6000$ W/m <sup>2</sup> K (A) $\leq 10000$ W/m <sup>2</sup> K (B)
DN 80 x 20 ( $d_i = 78 \times 20$ ) <div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;">  </div> <div style="text-align: center;">  </div> </div>	Dead leg: negligible Main flow: $\leq 70$ %	Dead leg: no relevant information Main flow: $\leq 10000$ W/m <sup>2</sup> K

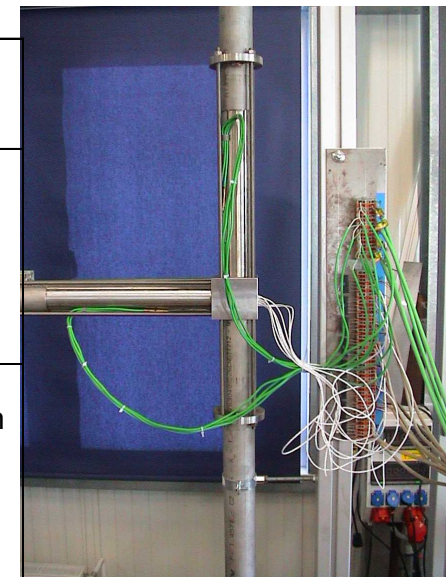


Figure 11: SPG, steel model, test results

# THERFAT – WP 2.2

# Deliverable D8

## Thermo-hydraulic tests with glass models (50 x 50 and 100 x 100)

- Steady flow in main pipe - one leg locked (closed valve) but leakage
- Temperature difference  $\Delta T$  simulated by different specific fluid densities
- Electrical conductivity measurement

- Results:
- “Temperature” alterations (percentage of  $\Delta T$ )
  - Report BLP –SB/50-04

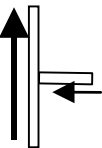
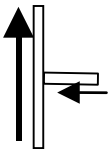
T and flow orientation		“Temp.” alterations
DN 50 x 50		Dead leg: $\leq 80 \%$
DN 100 x 100		Dead leg: $\leq 40 \%$



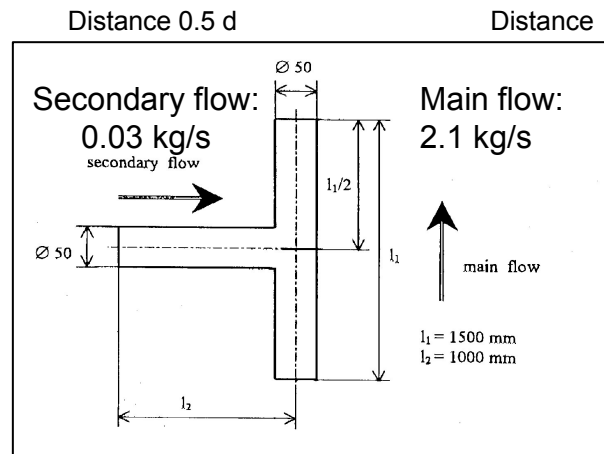
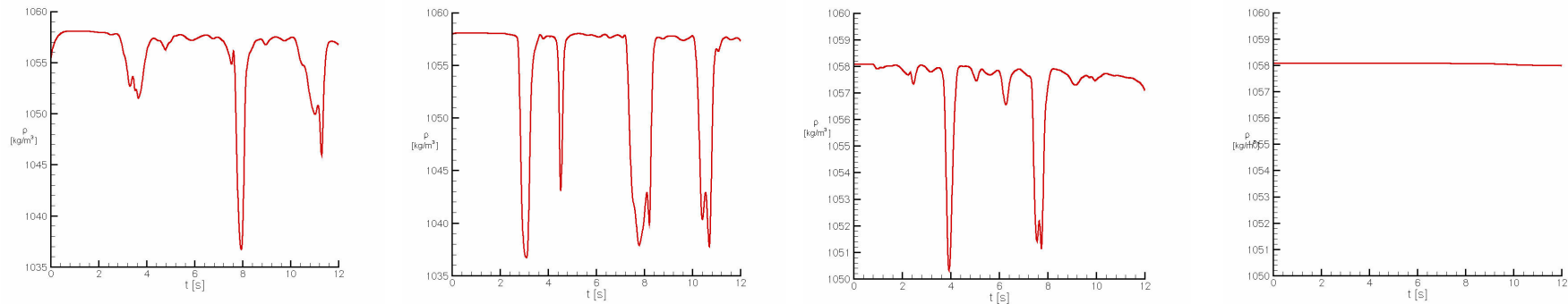
Figure 12: SPG, glass model, test results

# THERFAT – WP 2.3

# Deliverable D10/D11

## CFD benchmark calculation by Technical University of Dresden (TUD)

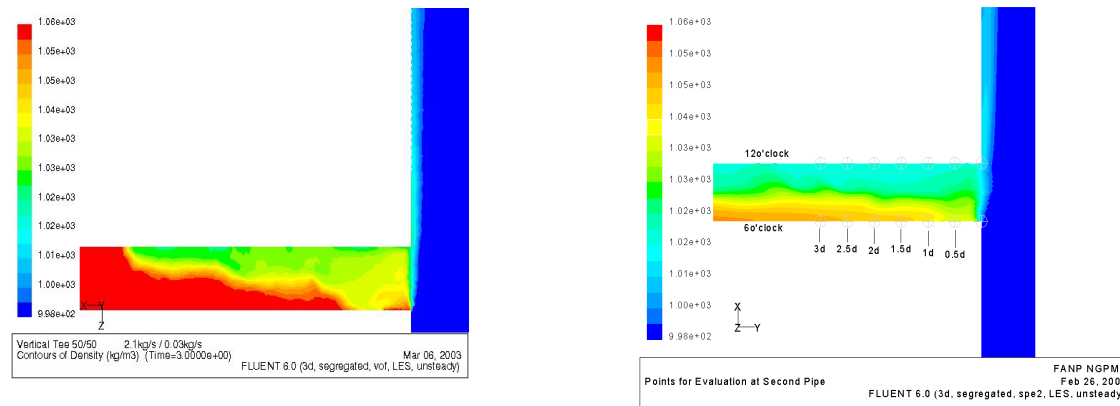
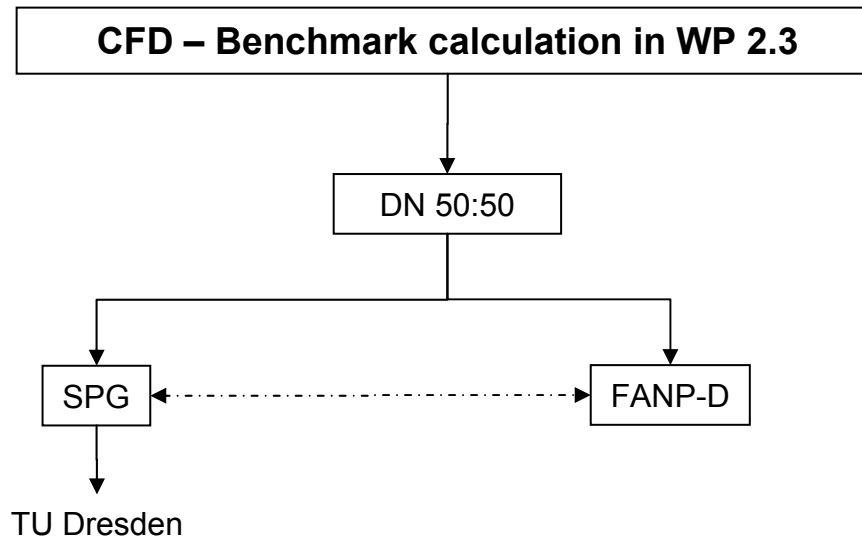
### Density versus time in the leakage pipe at 6-o'clock position



### Summary

- Qualitative agreement with test results (large peaks at low frequency between small amplitudes)
- Time period covered by calculation: 12 s (decay time for start-up effects in tests about 100 s)
- Relation costs/benefit too large

Figure 13: SPG, CFD benchmark analysis experiment/CFD analysis



**Figure 14: Benchmark of CFD analysis SPG, FANP-D**